

Fig. 1.

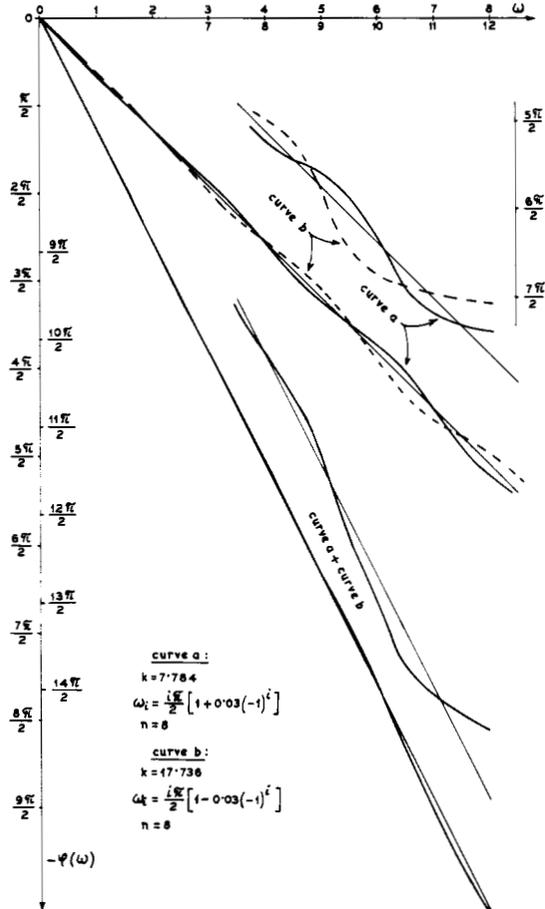


Fig. 2.

(10) and (11), in contrast to (5), (6) or (8), (9), give a wide spread in constant  $k$ . For the example at hand the following values for constant  $k$  have been found:

Curve a:

7.750; 7.784; 7.574; 7.985; 7.000; 8.290; 5.763; 7.957.

Curve b:

17.956; 17.736; 16.544; 15.782; 12.586; 11.472; 6.830; 3.412.

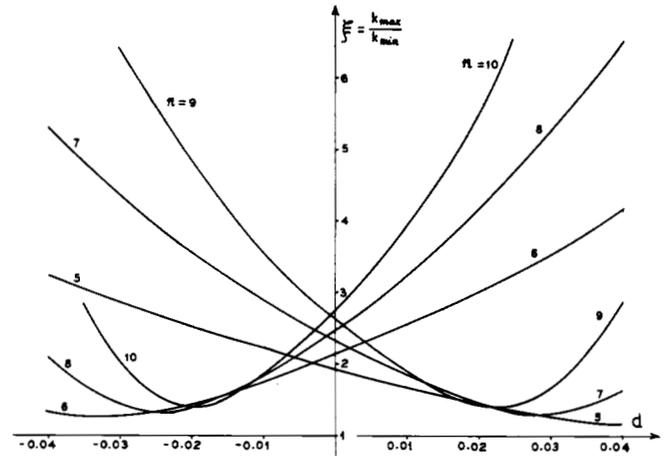


Fig. 3.

It is the large variation in constant  $k$  for curve  $b$  which prevents the cancellation of all the ripples.

If we designate  $k_{max}$  and  $k_{min}$  as the maximum and minimum values obtained for constant  $k$ , we can define the *constant  $k$  spread*

$$\xi = \frac{k_{max}}{k_{min}}$$

which may be used as an approximate measure of the quality of the linear phase approximation. For the example at hand, curve  $a$  with  $\xi = 1.44$  is a considerably better approximation than curve  $b$  with  $\xi = 5.26$ . Instead of using four relations (8) to (11) to define the zeros, we can use only one, and allow  $d$  to be a positive or negative real number. Now if we prescribe different values for  $d$  and calculate the resulting  $\xi$ , we obtain interesting curves in Fig. 3. It seems that the best value for displacement  $d$  is somewhere between 0.2 and 0.3 (or  $-0.2$  and  $-0.3$ ). The constant  $k$  spread is quite low (1.3 to 1.4) in that range, so the phase angle curve could be easily maintained within the limits of  $\pm 2$  to  $\pm 3$  percent.

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Pseudo-Series Combination of  $n$ -Port Networks

**Abstract**—The "pseudo-series" combination of two  $n$ -port networks is defined. A necessary and sufficient condition is given for the combined  $n$ -port network to have an open-circuit impedance matrix equal to the sum of the corresponding matrices of the component networks.

A problem that is of interest in the synthesis of  $n$ -port networks without transformers may be stated as follows. Given an open-circuit impedance matrix  $Z$ , what are the conditions under which  $Z$  may be expressed as the sum of  $Z_a, Z_b, \dots, Z_m$  such that each of the component matrices is conveniently realized by an  $n$ -port network, and such that a suitable combination of the component networks realizes the given  $Z$ -matrix? In this letter we define the pseudo-series combination of  $n$ -port networks<sup>(1)</sup> and give a necessary and sufficient condition for the  $Z$ -matrix of the combined network to be equal to the sum of the  $Z$ -matrices of the component networks.

We consider two connected networks  $N_a$  and  $N_b$  having only RLC ele-

ments and identical edge and port configurations. Let  $Z_a$  and  $Z_b$  be the open-circuit impedance matrices of  $N_a$  and  $N_b$ , respectively. From  $N_a$  and  $N_b$  we form a third  $n$ -port network  $N_c$  also having the same edge and port configurations and orientations, but having the impedance of each edge as the sum of the impedances of the corresponding edges of  $N_a$  and  $N_b$ . Then  $N_c$  is said to be the *pseudo-series combination* of  $N_a$  and  $N_b$ .<sup>[1]</sup> If the open-circuit impedance matrix  $Z_c$  of  $N_c$  is equal to  $Z_a + Z_b$ , then we qualify  $N_c$  as the *proper pseudo-series combination* of  $N_a$  and  $N_b$ .

Let  $Z_{ea}$  and  $Z_{eb}$  be the diagonal edge impedance matrices of the networks  $N_a$  and  $N_b$ . Let  $B = [B_1|B_2]$  be the common fundamental circuit matrix of  $N_a$  and  $N_b$  with respect to a tree which is so chosen that all the ports are included in a cotree, and let the rows of the submatrix  $B_1$  correspond to the port chords and those of  $B_2$  to the nonport chords. Then we have the following as the loop-impedance matrices of  $N_a$  and  $N_b$ :

$$\bar{Z}_a = \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} Z_{ea} [B_1|B_2]' = \begin{bmatrix} B_1 Z_{ea} B_1' & B_1 Z_{ea} B_2' \\ B_2 Z_{ea} B_1' & B_2 Z_{ea} B_2' \end{bmatrix} = \begin{bmatrix} Z_{11a} & Z_{12a} \\ Z_{21a} & Z_{22a} \end{bmatrix} \quad (1)$$

$$\bar{Z}_b = \begin{bmatrix} B_1 \\ B_2 \end{bmatrix} Z_{eb} [B_1|B_2]' = \begin{bmatrix} B_1 Z_{eb} B_1' & B_1 Z_{eb} B_2' \\ B_2 Z_{eb} B_1' & B_2 Z_{eb} B_2' \end{bmatrix} = \begin{bmatrix} Z_{11b} & Z_{12b} \\ Z_{21b} & Z_{22b} \end{bmatrix}. \quad (2)$$

Assuming that the  $Z_{22}$  matrices are nonsingular, the modified circuit matrices  $B_a$  and  $B_b$  for the networks  $N_a$  and  $N_b$ , as defined by Cederbaum<sup>[2]</sup> are given by

$$B_a = B_1 - Z_{12a} Z_{22a}^{-1} B_2 \quad (3)$$

$$B_b = B_1 - Z_{12b} Z_{22b}^{-1} B_2. \quad (4)$$

It can readily be shown that the pseudo-series combination of  $N_a$  and  $N_b$  is proper if their modified circuit matrices  $B_a$  and  $B_b$  are equal.<sup>[1]</sup> In what follows we show that the equality of the modified circuit matrices  $B_a$  and  $B_b$  is also a necessary condition in the general case for the proper pseudo-series combination of  $N_a$  and  $N_b$ .

Let the pseudo-series combination of  $N_a$  and  $N_b$  be proper, yielding the combined network  $N_c$ . We then have the following relations, where the vectors  $I_p$  and  $V_p$  refer to the port currents and voltages and the vector  $I_n$  refers to the currents in the nonport chords.

Network  $N_a$ :

$$V_{pa} = Z_{11a} I_p + Z_{12a} I_n \quad (5)$$

$$0 = Z_{21a} I_p + Z_{22a} I_n \quad (6)$$

Network  $N_b$ :

$$V_{pb} = Z_{11b} I_p + Z_{12b} I_n \quad (7)$$

$$0 = Z_{21b} I_p + Z_{22b} I_n. \quad (8)$$

Network  $N_c$ :

$$V_{pc} = (Z_{11a} + Z_{11b}) I_p + (Z_{12a} + Z_{12b}) I_n \quad (9)$$

$$0 = (Z_{21a} + Z_{21b}) I_p + (Z_{22a} + Z_{22b}) I_n. \quad (10)$$

In the foregoing, the matrices  $Z_{11a}$ ,  $Z_{11b}$ ,  $Z_{22a}$ , and  $Z_{22b}$  are symmetrical, and the matrices  $Z_{12a}$  and  $Z_{12b}$  are the transposes of the matrices  $Z_{21a}$  and  $Z_{21b}$ , respectively.

Since  $N_c$  is the proper pseudo-series combination of  $N_a$  and  $N_b$ , we have  $Z_c = Z_a + Z_b$ . For any arbitrary port current vector  $I_p$  we then have

$$V_{pc} = V_{pa} + V_{pb} \quad (11)$$

leading to the following relation:

$$Z_{12a} I_{na} + Z_{12b} I_{nb} = (Z_{12a} + Z_{12b}) I_{nc}. \quad (12)$$

Also, from (6), (8), and (10) we have

$$Z_{22a} I_{na} + Z_{22b} I_{nb} = (Z_{22a} + Z_{22b}) I_{nc}. \quad (13)$$

Premultiplying the terms in (12) by  $I_p'$  (the transpose of  $I_p$ ) and using (6) and (8), we obtain

$$I_{na}' Z_{22a} (I_{na} - I_{nc}) + I_{nb}' Z_{22b} (I_{nb} - I_{nc}) = 0. \quad (14)$$

Premultiplying the terms in (13) by  $I_{nc}'$ , we obtain

$$I_{nc}' Z_{22a} (I_{na} - I_{nc}) + I_{nc}' Z_{22b} (I_{nb} - I_{nc}) = 0. \quad (15)$$

From (14) and (15) we get

$$(I_{na} - I_{nc})' Z_{22a} (I_{na} - I_{nc}) + (I_{nb} - I_{nc})' Z_{22b} (I_{nb} - I_{nc}) = 0. \quad (16)$$

If the two matrices  $Z_{22a}$  and  $Z_{22b}$  are positive definite for positive real values of the complex frequency variable  $s$ , the only way in which (16) is satisfied is when both terms on the left-hand side are zero, i.e.,

$$I_{na} = I_{nb} = I_{nc}. \quad (17)$$

This leads to

$$Z_{22a}^{-1} Z_{21a} I_p = Z_{22b}^{-1} Z_{21b} I_p = (Z_{22a} + Z_{22b})^{-1} (Z_{21a} + Z_{21b}) I_p. \quad (18)$$

Since this is to be valid for all  $I_p$ , it follows that

$$Z_{12a} Z_{22a}^{-1} = Z_{12b} Z_{22b}^{-1} = (Z_{12a} + Z_{12b}) (Z_{22a} + Z_{22b})^{-1}. \quad (19)$$

Equation (19) is true not only for real positive values of  $s$ , but for all values of  $s$  by virtue of analytical continuation property. From (3), (4), and (19), it follows that the modified circuit matrices  $B_a$  and  $B_b$  of  $N_a$  and  $N_b$  are the same. It is also readily verified that  $N_c$  also has the same modified circuit matrix.

The foregoing discussion leads to the following theorem.

#### Theorem

The pseudo-series combination of two  $n$ -port networks  $N_a$  and  $N_b$  having nonsingular  $Z_{22}$  matrices that are positive definite for real positive values of the complex frequency variable  $s$  is proper if and only if the modified circuit matrices of  $N_a$  and  $N_b$  are equal.

It is well known that the principal minors of the loop-impedance matrices of RLC networks containing only positive resistances, inductances, and capacitances are positive definite or positive semidefinite for real positive values of  $s$ . For the  $Z$ -matrix to exist, however, the  $Z_{22}$  matrices should be nonsingular and hence positive definite for real positive values of  $s$ . Hence the criterion contained in the theorem is generally applicable to such networks.

The extension of the foregoing result to more than two  $n$ -port networks is obvious. A straightforward application of this criterion to test for the proper pseudo-series combination of  $p$  networks requires the inversion of  $p$   $Z_{22}$  matrices. It can be shown, however, that the inversion of one such matrix will do for this purpose. A convenient test procedure incorporating this criterion is given elsewhere.<sup>[3]</sup>

Lempel and Cederbaum<sup>[4]</sup> have recently given a similar necessary and sufficient condition in terms of the modified cut-set matrix for the proper parallel interconnection of  $n$ -port networks without internal vertices. It can be shown that if one considers the pseudo-parallel combination instead of the regular parallel interconnection (the internal vertices are also interconnected in the pseudo-parallel combination), then the same criterion is also valid for  $n$ -port networks with internal vertices.

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