

Sensitivity Invariants for Linear Time-Invariant Networks

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Abstract—For a general linear time-invariant network it is shown that the sum of the sensitivities, of any order, of a network function over different parameter sets is invariant. An expression is derived for calculating the sum of $(k+1)$ th-order sensitivities knowing the same for k th-order sensitivities. It is also shown that lower bounds for the quadratic sensitivity index may be obtained by using the first-order sensitivity invariants.

I. INTRODUCTION

THE CONJECTURE of Leeds and Ugron [1] that the sum of the sensitivity functions (over all components of each continuously equivalent network) is invariant, with respect to various equivalent networks, has led to a number of investigations on the invariant nature of the sum of the sensitivities of a network function. A good survey of these investigations is available in [2], [3]. Recently, Sablatash and Seviora [4] have used Tellegen's theorem and the concept of the adjoint or transpose of a network [5]–[7] to establish the invariant nature of the sum of the sensitivities of network functions of a certain class of networks containing uniformly distributed \overline{RC} and lossless lines. Similar invariance results may be established for networks that in addition include active elements, as well as tapered lines, by either following Blostein's approach [8] or the adjoint approach [9]. We first briefly summarize these results, show how these may be used to obtain lower bounds for Schoefler's [10] quadratic sensitivity index, and then establish the invariant nature of the sum of the higher order sensitivities of network functions over different sets of parameters.

II. SENSITIVITY INVARIANTS AND QUADRATIC SENSITIVITY INDEX

Consider a general n -port network N consisting of lumped resistors ($R_i=1/G_i$), inductors ($L_i=1/\Gamma_i$), capacitors ($C_i=1/D_i$), gyrators, controlled sources [current to voltage transducers (CVT's), voltage to current transducers (VCT's), voltage to voltage transducers (VVT's), and current to current transducers (CCT's)], negative impedance converters (NIC's), lossless tapered lines, and \overline{RC} tapered lines. Let the impedance matrix of a gyrator be denoted by

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$$\begin{bmatrix} 0 & \alpha_{i1} \\ \alpha_{i2} & 0 \end{bmatrix}$$

and the parameters of a nonuniform transmission line (NUTL) be given as follows:

$$\begin{aligned} \overline{Z}_i(s, x) &= Z_{0i}(s)f(x) \\ \overline{Y}_i(s, x) &= Y_{0i}(s)g(x), \quad a \leq x \leq b \end{aligned}$$

where $\overline{Z}_i(s, x)$ and $\overline{Y}_i(s, x)$ are series impedance per unit length and shunt admittance per unit length of a general NUTL. A lossless NUTL is described by

$$\begin{aligned} \overline{L}_i &= L_{0i}f(x) \\ \overline{C}_i &= C_{0i}g(x), \quad a \leq x \leq b \end{aligned}$$

and a tapered \overline{RC} line by

$$\begin{aligned} \overline{R}_i &= R_{0i}f(x) \\ \overline{C}_i &= C_{0i}g(x), \quad a \leq x \leq b. \end{aligned}$$

Let

$$D_{0i} = 1/C_{0i}$$

and

$$Z_{\overline{LC}i} = \sqrt{\frac{L_{0i}}{C_{0i}}} = \frac{1}{Y_{\overline{LC}i}} \quad \text{and} \quad Z_{\overline{RC}i} = \sqrt{\frac{R_{0i}}{C_{0i}}} = \frac{1}{Y_{\overline{RC}i}}$$

be the "characteristic impedance" of a lossless NUTL and "characteristic impedance" of a tapered \overline{RC} line, respectively. Further, let $r_i=1/g_i$ and $\delta_i=1/\gamma_i$ be the transfer resistance of a CVT and transfer conductance of a VCT, respectively.

For the network N , if p_k is a member of the set,

$P = \{p_k\} = \{R_i, L_i, D_i, (\alpha_{i1}, \alpha_{i2}), (R_{0i}, D_{0i}), Z_{\overline{LC}i}, r_i, \gamma_i\}$ where the subset (R_{0i}, D_{0i}) may be replaced by $Z_{\overline{RC}i}$, while the subset $Z_{\overline{LC}i}$ by (L_{0i}, D_{0i}) ; then we have [9]

$$\sum_{p_k} \frac{p_k}{Z_{ij}} \frac{\partial Z_{ij}}{\partial p_k} = 1 \quad (1)$$

$$\sum_{p_k} \frac{p_k}{Y_{ij}} \frac{\partial Y_{ij}}{\partial p_k} = -1 \quad (2)$$

$$\sum_{p_k} p_k \frac{\partial T}{\partial p_k} = 0 \quad (3)$$

$$\sum_{p_k} p_k \frac{\partial S}{\partial p_k} = \frac{1}{2} (U - S^2) \quad (4)$$

$$\sum_{p_{k'}} p_{k'} \frac{\partial S}{\partial p_{k'}} = 0 \quad (5)$$

where Z_{ij} is the transfer impedance between the i th and j th ports of N , Y_{ij} is the transfer admittance, T is the open-circuit voltage ratio or short-circuit current ratio, S is the scattering matrix, U is the unit matrix, and $\{p_k'\} = \{p_k\} \cup \{\rho_i, \text{ the normalizing resistors}\}$.

It can also be shown [9] that for the network N , over the subset $M = \{m_k\} = \{L_i, C_i, (L_{0i}, C_{0i})\}$, the summed sensitivity of a network function F is given by

$$\sum_{m_k} \frac{m_k}{F} \frac{\partial F}{\partial m_k} = \frac{s}{F} \frac{\partial F}{\partial s} \quad (6)$$

For a network N_1 consisting of lumped resistors, capacitors, gyrators, \overline{RC} tapered lines, controlled sources, and NIC's, if q_k is a member of the set $Q = \{q_k\} = \{R_i, C_i, (\alpha_{i1}, \alpha_{i2}), (R_{0i}, C_{0i}), r_i, \gamma_i\}$, then it can be shown that [9]

$$\sum_{q_k} \frac{q_k}{Z_{ij}} \frac{\partial Z_{ij}}{\partial q_k} = \frac{2s}{Z_{ij}} \frac{\partial Z_{ij}}{\partial s} + 1 \quad (7)$$

$$\sum_{q_k} \frac{q_k}{Y_{ij}} \frac{\partial Y_{ij}}{\partial q_k} = \frac{2s}{Y_{ij}} \frac{\partial Y_{ij}}{\partial s} - 1 \quad (8)$$

$$\sum_{q_k} \frac{q_k}{T} \frac{\partial T}{\partial q_k} = \frac{2s}{T} \frac{\partial T}{\partial s} \quad (9)$$

$$\sum_{q_k} q_k \frac{\partial S}{\partial q_k} = 2s \frac{\partial S}{\partial s} + \frac{1}{2} (U - S^2) \quad (10)$$

$$\sum_{q_k'} q_k' \frac{\partial S}{\partial q_k'} = 2s \frac{\partial S}{\partial s} \quad (11)$$

where $\{q_k'\} = \{q_k\} \cup \{\rho_i\}$.

Using the approach of Kasper and Schmidt [11], the different invariances given in this section may be used as constraints in minimizing the quadratic sensitivity index

$$\phi = \sum_{p_k} |S_{p_k}^F|^2$$

where

$$S_{p_k}^F = \frac{p_k}{F} \frac{\partial F}{\partial p_k}$$

For the different networks considered in this section, some of the lower bounds are as follows.

1) For network N ,

$$\phi = \sum_{p_k} |S_{p_k}^F|^2 \geq \frac{1}{n}$$

where F is Z_{ij} or Y_{ij} and n is the total number of elements in the set $\{p_k\}$.

2) For network N_1 ,

$$\phi = \sum_{q_k} |S_{q_k}^{Z_{ij}}|^2 \geq \frac{1}{n_1} |S_s^{Z_{ij}} + 1|^2 + \frac{1}{n_2} |S_s^{Z_{ij}}|^2$$

$$\phi = \sum_{q_k} |S_{q_k}^{Y_{ij}}|^2 \geq \frac{1}{n_1} |S_s^{Y_{ij}} - 1|^2 + \frac{1}{n_2} |S_s^{Y_{ij}}|^2$$

$$\phi = \sum_{q_k} |S_{q_k}^T|^2 \geq \left(\frac{1}{n_1} + \frac{1}{n_2}\right) |S_s^T|^2$$

where n_1 and n_2 are the number of elements in the sets $\{q_{k1}\} = \{R_i, (\alpha_{i1}, \alpha_{i2}), R_{0i}, r_i, \gamma_i\}$ and $\{q_{k2}\} = \{C_i, C_{0i}\}$, respectively.

3) For a network N_2 consisting of lumped capacitors, inductors, lossless tapered lines, VVT's, CCT's and NIC's,

$$\phi = \sum_{m_k} |S_{m_k}^{Z_{ij}}|^2 \geq \frac{1}{4n_1} |S_s^{Z_{ij}} - 1|^2 + \frac{1}{4n_2} |S_s^{Z_{ij}} + 1|^2$$

$$\phi = \sum_{m_k} |S_{m_k}^{Y_{ij}}|^2 \geq \frac{1}{4n_1} |S_s^{Y_{ij}} + 1|^2 + \frac{1}{4n_2} |S_s^{Y_{ij}} - 1|^2$$

$$\phi = \sum_{m_k} |S_{m_k}^T|^2 \geq \frac{1}{4} \left(\frac{1}{n_1} + \frac{1}{n_2}\right) |S_s^T|^2$$

where n_1 and n_2 are, respectively, the number of elements in $\{m_{k1}\} = \{C_i, C_{0i}\}$ and $\{m_{k2}\} = \{L_i, L_{0i}\}$.

It may be observed from the above expressions that as the number of elements is increased, the lower bounds decrease, thereby strengthening the conjecture of Leeds and Ugron [1].

III. HIGHER ORDER SENSITIVITY INVARIANTS

We now establish the invariant nature of the sum of the second-order sensitivities of network functions.

For the network N , over the set $\{p_k\}$ from (1),

$$Z = \sum_{k=1}^n p_k \frac{\partial Z}{\partial p_k} \quad (12)$$

In writing the above expression it is assumed that the set $\{p_k\}$ consists of n elements $p_k, k=1, 2, \dots, n$.

From (12),

$$\sum_{i=1}^n p_i \frac{\partial Z}{\partial p_i} = \sum_{i=1}^n \sum_{k=1}^n p_i p_k \frac{\partial^2 Z}{\partial p_i \partial p_k} + \sum_{i=1}^n \sum_{k=1}^n p_i \frac{\partial}{\partial p_i} (p_k) \frac{\partial Z}{\partial p_k} \quad (13)$$

Since

$$\frac{\partial p_k}{\partial p_i} = \begin{cases} 0, & \text{if } i \neq k \\ 1, & \text{if } i = k \end{cases}$$

it is readily seen that the second term on the right-hand side of (13) is equal to $\sum_{i=1}^n p_i (\partial Z / \partial p_i)$. Thus it follows from (13) that

$$\sum_{i=1}^n \sum_{k=1}^n p_i p_k \frac{\partial^2 Z}{\partial p_i \partial p_k} = 0 \quad (14)$$

That is, the sum of second-order sensitivities of the impedance matrix Z of the network N is invariant over the set $\{p_k\}$.

For the admittance matrix \mathbf{Y} , current or voltage transfer function T , and scattering matrix \mathbf{S} , it can be shown that

$$\sum_{i=1}^n \sum_{k=1}^n p_i p_k \frac{\partial^2 \mathbf{Y}}{\partial p_i \partial p_k} = 2\mathbf{Y} \quad (15)$$

$$\sum_{i=1}^n \sum_{k=1}^n p_i p_k \frac{\partial^2 T}{\partial p_i \partial p_k} = 0 \quad (16)$$

$$\sum_{i=1}^n \sum_{k=1}^n p_i p_k \frac{\partial^2 \mathbf{S}}{\partial p_i \partial p_k} = -\frac{1}{2}(\mathbf{U} + \mathbf{S})(\mathbf{U} - \mathbf{S}^2) \quad (17)$$

$$\sum_{p_i' \in \{p_k'\}} \sum_{p_k' \in \{p_k'\}} p_i' p_k' \frac{\partial^2 \mathbf{S}}{\partial p_i' \partial p_k'} = 0. \quad (18)$$

Similarly, it can be shown that for the network N , over the set $\{m_k\}$,

$$\sum_{i=1}^n \sum_{k=1}^n m_i m_k \frac{\partial^2 F}{\partial m_i \partial m_k} = s^2 \frac{\partial^2 F}{\partial s^2} \quad (19)$$

where m_i and m_k are the members of the set $\{m_k\}$ and F is an impedance or admittance parameter or voltage or current transfer function. The same relationship holds good even if F is a \mathbf{Z} - or \mathbf{Y} -matrix.

Consider next the network N_1 , over the set $\{q_k\}$. Let the set $\{q_k\}$ consist of n elements q_k , $k=1, 2, \dots, n$. From (7),

$$\sum_{k=1}^n q_k \frac{\partial \mathbf{Z}}{\partial q_k} = 2s \frac{\partial \mathbf{Z}}{\partial s} + \mathbf{Z}. \quad (20)$$

Following the same procedure as outlined earlier, the following can be proved using (7)–(11):

$$\sum_{i=1}^n \sum_{k=1}^n q_i q_k \frac{\partial^2 \mathbf{Z}}{\partial q_i \partial q_k} = 6s \frac{\partial \mathbf{Z}}{\partial s} + 4s^2 \frac{\partial^2 \mathbf{Z}}{\partial s^2} \quad (21)$$

$$\sum_{i=1}^n \sum_{k=1}^n q_i q_k \frac{\partial^2 \mathbf{Y}}{\partial q_i \partial q_k} = 4s^2 \frac{\partial^2 \mathbf{Y}}{\partial s^2} - 2s \frac{\partial \mathbf{Y}}{\partial s} + 2\mathbf{Y} \quad (22)$$

$$\sum_{i=1}^n \sum_{k=1}^n q_i q_k \frac{\partial^2 T}{\partial q_i \partial q_k} = 2s \frac{\partial T}{\partial s} + 4s^2 \frac{\partial^2 T}{\partial s^2} \quad (23)$$

$$\sum_{i=1}^n \sum_{k=1}^n q_i q_k \frac{\partial^2 \mathbf{S}}{\partial q_i \partial q_k} = 4s^2 \frac{\partial^2 \mathbf{S}}{\partial s^2} + 2s \frac{\partial \mathbf{S}}{\partial s} - 4s \cdot \mathbf{S} \frac{\partial \mathbf{S}}{\partial s} - \frac{1}{2}(\mathbf{U} - \mathbf{S}^2) - \frac{\mathbf{S}}{2}(\mathbf{U} - \mathbf{S}^2) \quad (24)$$

$$\sum_{q_i' \in \{q_k'\}} \sum_{q_k' \in \{q_k'\}} q_i' q_k' \frac{\partial^2 \mathbf{S}}{\partial q_i' \partial q_k'} = 4s^2 \frac{\partial^2 \mathbf{S}}{\partial s^2} + 2s \frac{\partial \mathbf{S}}{\partial s}. \quad (25)$$

We conclude this section with a general result that will help in obtaining the sum of the $(k+1)$ th-order sensitivities of a network function from the sum of the k th-order sensitivities.

Consider any network function $F(p_1, p_2, \dots, p_n)$. Let X_k be the k th-order summed sensitivity and X_{k+1}

the $(k+1)$ th-order summed sensitivity; then

$$X_k = \sum_{i_k=1}^n \sum_{i_{k-1}=1}^n \cdots \sum_{i_2=1}^n \sum_{i_1=1}^n p_{i_1} p_{i_2} \cdots p_{i_k} \frac{\partial^k F}{\partial p_{i_1} \partial p_{i_2} \cdots \partial p_{i_k}} \quad (26)$$

and

$$X_{k+1} = \sum_{i_{k+1}=1}^n \sum_{i_k=1}^n \cdots \sum_{i_2=1}^n \sum_{i_1=1}^n p_{i_1} p_{i_2} \cdots p_{i_{k+1}} \frac{\partial^{k+1} F}{\partial p_{i_1} \partial p_{i_2} \cdots \partial p_{i_{k+1}}}. \quad (27)$$

From (26),

$$\sum_{i_{k+1}=1}^n p_{i_{k+1}} \frac{\partial X_k}{\partial p_{i_{k+1}}} = X_{k+1} + \sum_{i_k=1}^n \sum_{i_{k-1}=1}^n \cdots \sum_{i_2=1}^n \sum_{i_1=1}^n \frac{\partial^k F}{\partial p_{i_1} \partial p_{i_2} \cdots \partial p_{i_k}} \sum_{i_{k+1}=1}^n p_{i_{k+1}} \frac{\partial (p_{i_1} p_{i_2} \cdots p_{i_k})}{\partial p_{i_{k+1}}}. \quad (28)$$

In the second term of the right-hand side of (28), k parameters are taken at a time, but some of the parameters may occur more than once. Let a typical term of $(p_{i_1} p_{i_2} \cdots p_{i_k})$ be

$$p_{i_1}^{x_{i_1}} p_{i_2}^{x_{i_2}} \cdots p_{i_k}^{x_{i_k}} \triangleq A, \quad ij \in \{1, 2, \dots, n\}. \quad (29)$$

It should be noted that $\sum_{j=1}^k x_{ij} = k$. Then,

$$p_{ij} \frac{\partial}{\partial p_{ij}} (A) = \begin{cases} 0, & \text{if } x_{ij} = 0 \\ x_{ij} A, & \text{if } x_{ij} \neq 0. \end{cases} \quad (30)$$

Hence

$$\sum_{j=1}^n p_{ij} \frac{\partial (A)}{\partial p_{ij}} = A \sum_{j=1}^k x_{ij} = kA. \quad (31)$$

Using (31) in (28),

$$\sum_{i_{k+1}=1}^n p_{i_{k+1}} \frac{\partial X_k}{\partial p_{i_{k+1}}} = X_{k+1} + kX_k \quad (32)$$

or

$$X_{k+1} = \sum_{i=1}^n p_i \frac{\partial X_k}{\partial p_i} - kX_k.$$

Equation (32) expresses the $(k+1)$ th-order summed sensitivity in terms of the summed k th-order sensitivity.

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Single-Transistor All-Pass Networks

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Abstract—A network configuration consisting of a resistive two-port bridged by a lossless one-port is considered. It is shown that in certain cases this configuration is capable of realizing a voltage transfer function equal to that of a constant-resistance passive lattice. As a special case, conditions are derived on the two-port parameters for the structure to be all pass. It is determined that a single transistor suffices to realize the two-port network, thus resulting in a very simple all-pass structure; only one coil, one capacitor, and one transistor are necessary to realize a second-degree all-pass voltage transfer function. Higher order transfer functions can be realized by adding an LC branch per each additional second-order factor to the same transistor circuit. In the second-order case, losses in the coil can be compensated. In higher order realizations coil losses cannot be compensated, but a design technique which achieves an arbitrarily close approximation to the desired all-pass transfer function is presented. Methods of cascading lower order sections are discussed and experimental results are given.

INTRODUCTION

MODERN more stringent requirements of communication networks, such as increasing their bandwidth, pose special problems in the design of phase equalizers.

Passive realizations suffer from many drawbacks, the most important of which are 1) an excessive number of coils and capacitors, 2) lack of unbalanced transformerless sections for certain values of pole Q [1], and 3) finite component Q 's make it impossible to conform to stringent specifications on the amplitude characteristic.

Realizations using active elements, namely, transistors in operational amplifiers [2] or gyrators [3], wherein the active components determine the locations of the poles and zeros, can be used over a limited fre-

quency range only. The bandwidth limitation is due in this case to the large number of transistors needed in the implementation of the operational amplifier or the gyrator.

A circuit which overcomes to a certain extent the bandwidth limitation is being developed at this time [4], but it needs one differential input amplifier of a high common-mode rejection ratio.

Two realization methods requiring only one transistor may be found in the literature. The circuit proposed by Allemandou [5] suffers from limited bandwidth and accuracy due to the fact that its performance depends on the emitter and collector voltages being equal in magnitude and opposite in phase.

Aronhime [6] describes only one application of the single-transistor circuit, namely, its use as a first-order all-pass network. It is shown in this paper that this circuit can be used for the realization of any transfer function that can be realized by a passive lattice. The method presented leads to considerable savings in the number of reactive components; it enables the designer to compensate for the inevitable losses in these components and results in a broad-band realization of the desired transfer function.

THE GENERAL CONFIGURATION

Consider a configuration consisting of a resistive unbalanced two-port N_a with the short-circuit admittance matrix

$$Y_a = \begin{bmatrix} G_1 & G_2 \\ G_3 & G_4 \end{bmatrix} \quad (1)$$

bridged by a one-port N_b of admittance Y . The voltage